

## CO-DIFFUSION FOR P-TYPE PERT SOLAR CELLS USING APCVD BSG LAYERS AS BORON DOPING SOURCE

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**ABSTRACT:** In this work, we investigate boron-doped back surface field (BSF) formation from borosilicate glass (BSG) deposited by atmospheric pressure chemical vapor deposition (APCVD). Carrier lifetime samples with different boron concentration in the BSG are exposed to high-temperature processes with varying temperature and gas atmospheres. The development aims at producing p-type Si-based passivated emitter and rear totally diffused (PERT) cells in a POCl<sub>3</sub> co-diffusion process. Our experiments confirm the critical impact of the O<sub>2</sub> concentration on boron diffusion from APCVD BSG layers. For different peak temperatures Si surface oxidation formation need to be balanced carefully. Moderate diffusion temperatures of 875°C (30 min) yield a BSF doping with  $R_{sh} = 131 \Omega/\text{sq}$  and a recombination current density of  $J_{0,BSF} = 21 \text{ fA}/\text{cm}^2$  (planar surface, AlO<sub>x</sub>/SiN<sub>x</sub>-passivation). Finally, 156 mm sized PERT cells fabricated from p-type Czochralski-grown Si wafers using the developed co-diffusion process show peak efficiencies of 20.6%, confirming the feasibility of our co-diffusion approach.

**Keywords:** APCVD, boron-doping, BSG, PERT, co-diffusion

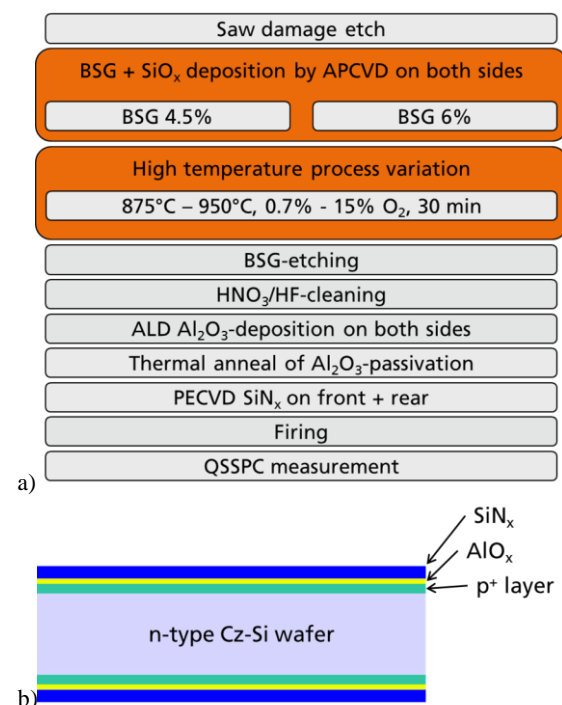
### 1 INTRODUCTION

Bifacial passivated emitter and rear (PERC) solar cells allow for conversion efficiencies beyond 21% while enabling bifacial module designs [1]. The bifacial operation allows for increasing the energy yield or a broadening of the energy output over a day, depending on the physical surrounding and module placement [2]. Currently, bifacial PERC cells reach rear efficiencies of 16.7%, where the high shading loss of the rear aluminum grid is a major limitation [1]. One approach to reduce these losses is to use a passivated emitter and rear totally diffused (PERT) cell structure that allows significantly higher rear finger spacing due to additional lateral conductance of the back surface field (BSF). In addition, PERT cells tolerate high resistivity wafers, which reduce light induced degradation (LID) due to boron-oxygen complex recombination [3]. In state of the art processing emitter and BSF of PERT solar cells are formed using sequential diffusion processes with POCl<sub>3</sub> and BBr<sub>3</sub> as liquid dopant precursor [4–6]. The additional diffusion step compared to PERC manufacturing implicates additional process complexity and cost. To avoid this additional effort, we present a fast and cost-effective approach to form the phosphorus-doped emitter and boron-doped BSF in one single co-diffusion process. Therefore we investigate co-diffusion from POCl<sub>3</sub> atmosphere and a pre deposited borosilicate glass (BSG) layer by atmospheric pressure chemical vapor deposition (APCVD). Main advantage of this approach is its industrial feasibility while keeping the flexibility to independently adjust doping profiles [7].

This paper first discusses the development of a POCl<sub>3</sub>-based co-diffusion tube furnace process suitable for the fabrication of p-type PERT solar cells. Finally, we prove the co-diffusion concept by fabricating monofacial PERT solar cells from p-type Czochralski-grown silicon (Cz-Si) wafers.

### 2 APPROACH

#### 2.1 Boron-doping from APCVD BSG layers

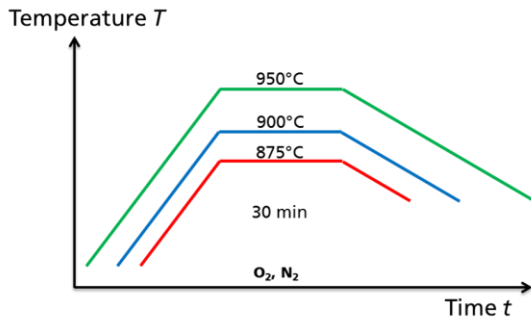


**Fig. 1:** a) Process sequence and b) sample design for symmetric samples used to characterize boron diffused surfaces made from APCVD BSG layers.

We first investigate boron-doping for BSF formation from APCVD BSG layers with respect to sheet resistance, doping profile and carrier recombination. Fig. 1 represents a) the process scheme and b) the sample design used to develop boron diffusion from APCVD BSG layers.

We use n-type Cz-Si wafers with base resistivity  $\rho_B = 2.2 \Omega\text{cm}$  (determined after thermal processing) and

an edge length of 156 mm for symmetric carrier lifetime samples. Another set of n-type Cz-Si wafers is selected for four point probe (4pp) and electrochemical capacitance voltage (ECV) measurements. All wafers receive a saw damage etch. Then, the deposition of the



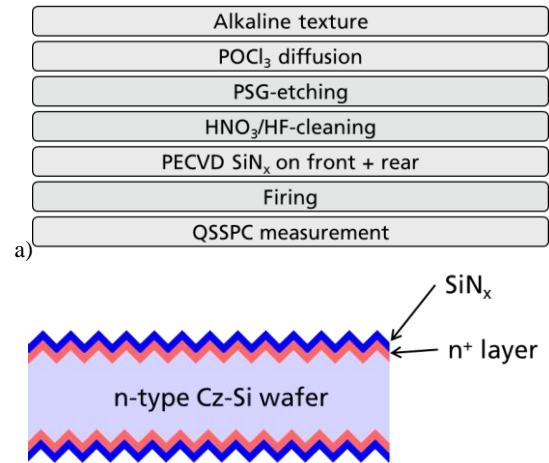
**Fig. 2:** Schematic of the applied high temperature processes. Peak temperatures  $T_{\text{Peak}} = 875^{\circ}\text{C}$ ,  $T_{\text{Peak}} = 900^{\circ}\text{C}$ , and  $T_{\text{Peak}} = 950^{\circ}\text{C}$  are used for a plateau time of 30 minutes. During whole diffusion process the  $\text{O}_2$  concentration is kept constant. Different  $\text{O}_2$  concentrations from 0% to 3% are investigated.

BSG/ $\text{SiO}_x$  layer stack in one deposition is realized by APCVD on both sides of the wafer. We apply two different boron-contents of the BSG layer (nominally 4.5% and 6%). Then, diffusion temperatures  $T_{\text{Peak}} = 875^{\circ}\text{C}$ ,  $T_{\text{Peak}} = 900^{\circ}\text{C}$ , and  $T_{\text{Peak}} = 950^{\circ}\text{C}$  (all with 30min plateau) at different  $\text{O}_2$  concentrations in the atmosphere are applied. Fig. 2 presents a scheme of the high temperature processes.

Following the high temperature step, the BSG/ $\text{SiO}_x$  layers are removed in HF solution and 4pp and ECV measurements yield sheet resistance  $R_{\text{sh}}$  and doping profile, respectively. The symmetric carrier lifetime samples receive wet chemical cleaning with a  $\text{HNO}_3/\text{HF}$  sequence, both-sided surface passivation by atomic layer deposition (Fast-ALD) of an  $\text{Al}_2\text{O}_3$  layer and subsequent out gassing as well as a plasma enhanced chemical vapor deposited (PECVD)  $\text{SiN}_x$  capping. A fast firing process activates the passivation. Finally quasi steady state photo conductance (QSSPC) measurement determine the dark saturation current  $J_{0,\text{BSF}}$  using the procedure from Ref. [8].

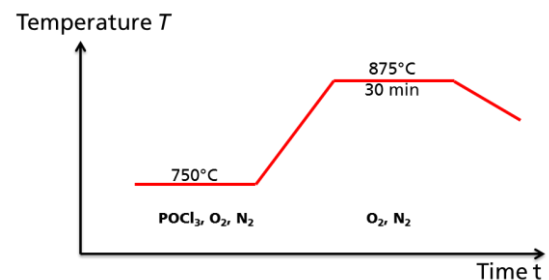
## 2.2 Co-diffusion

Based on a high temperature process with  $T_{\text{Peak}} = 875^{\circ}\text{C}$ , a  $\text{POCl}_3$ -based co-diffusion process is developed. Fig. 3 shows a) the process scheme and b) the sample design.



**Fig. 3:** a) Process sequence and b) sample design used to characterize phosphorus diffused surfaces from  $\text{POCl}_3$ -based co-diffusion process with respect to carrier recombination.

First, n-type Cz-Si wafers with  $\rho_B = 2.2 \Omega\text{cm}$  (determined after thermal processing) and an edge length of 156 mm are alkaline textured. Then, a  $\text{POCl}_3$ -based diffusion with  $T_{\text{Peak}} = 875^{\circ}\text{C}$  (30min plateau) is applied (see Fig. 4).



**Fig. 4:** Schematic of the investigated  $\text{POCl}_3$ -based co-diffusion process.

After phosphosilicate glass (PSG) removal, 4pp and ECV measurements are realized using saw damage etched n-type Si-reference wafers. These wafers are processed in parallel to alkaline textured Si wafers. The textured symmetric n-type Cz-Si lifetime samples receive wet chemical cleaning with a  $\text{HNO}_3/\text{HF}$  sequence, PECVD  $\text{SiN}_x$  passivation and firing. Finally, QSSPC measurements determine emitter saturation current  $J_{0e}$ ; see Ref. [8].

### 2.3 Solar cell fabrication

Fig. 5 represents a process sequence for the fabrication of p-type PERC and co-diffused PERT solar cells.

PERC reference	Co-diffused PERT
Alkaline texture	
Single side wet chemical polish	
	BSG + SiO <sub>x</sub> by APCVD on rear
	Single side HF cleaning on front
POCl <sub>3</sub> -diffusion	POCl <sub>3</sub> -Co-diffusion
CEI on rear + PSG etching	BSG/PSG-etching
HNO <sub>3</sub> /HF-cleaning	
ALD Al <sub>2</sub> O <sub>3</sub> -deposition on rear side	
Thermal anneal of Al <sub>2</sub> O <sub>3</sub> -passivation	
PECVD SiN <sub>x</sub> on front + rear	
Local laser contact opening LCO on rear side	
Full area al screen printing on rear side	
Ag double screen printing on front side	
Firing	
IV measurement	

**Fig. 5:** Process sequence for fabricating PERC (left) and PERT (right) type solar cells.

P-type Cz-Si wafers with an edge length of 156 mm,  $\rho_B = 2.9 \Omega\text{cm}$  and an initial thickness  $W = 180 \mu\text{m}$  are textured in an alkaline solution. In a second step the rear side texture is smoothed by a single side wet chemical polish.

For the PERT cells, a BSG/SiO<sub>x</sub> layer system is deposited on the polished rear surface by APCVD in one single process, followed by a single side HF cleaning sequence for the non-deposited front side. The wafers are then subjected to a POCl<sub>3</sub>-based co-diffusion tube furnace process to simultaneously form a phosphorus doped emitter on the front side and a boron doped BSF on the rear side of the PERT cell. An HF bath then removes the formed PSG and BSG layers.

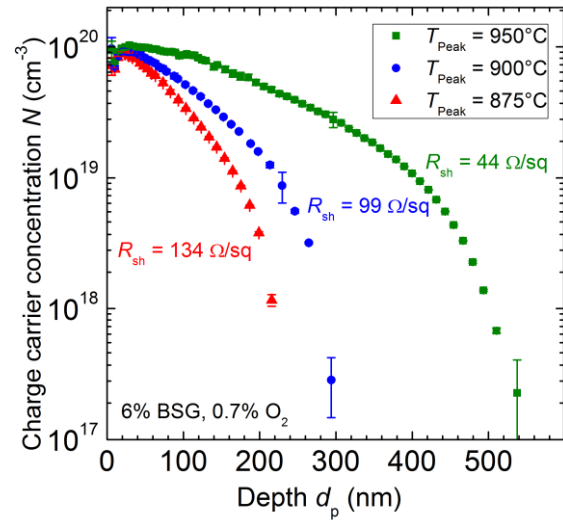
In contrast, the PERC reference cells are directly subjected to a standard POCl<sub>3</sub>-diffusion process [9]. The rear side of PERC cell is then subjected to wet chemical edge isolation (CEI) followed by front PSG removal.

PERC and PERT cells thus differ in diffusion sequence; however, after diffusion their fabrication is similar. Rear passivation is realized by an Al<sub>2</sub>O<sub>3</sub> layer deposited by Fast-ALD followed by thermal anneal of the Al<sub>2</sub>O<sub>3</sub> layer. Then a SiN<sub>x</sub> layer is deposited on top of the Al<sub>2</sub>O<sub>3</sub> layer. The phosphorus doped emitter at the front side is passivated by a SiN<sub>x</sub> layer deposited by PECVD. Then, local contact opening (LCO) of line shaped rear contacts is realized by a laser process and a full-area aluminum paste is applied by screen-printing. Note that for both PERC and PERT cells an identical line pitch of 700  $\mu\text{m}$  is chosen (optimized for the PERC structure). The emitter side is subjected to a double screen printing step using a commercially available silver paste. Final steps are contact formation by a firing step in a commercial fast firing oven (variation of peak temperature) and IV measurement using an industrial cell tester.

## 3 RESULTS

### 3.1 Influence of peak temperature on boron concentration

Fig. 6 presents boron doping profiles for BSG layers with 6% boron concentration from diffusions with  $T_{\text{Peak}} = 875^\circ\text{C}$ ,  $T_{\text{Peak}} = 900^\circ\text{C}$ , and  $T_{\text{Peak}} = 950^\circ\text{C}$ , all with an O<sub>2</sub> concentration of 0.7% in the diffusion atmosphere (see Fig. 2 for the schematic of the high-temperature processes). The used samples are fabricated as described in section 2.1, see Fig. 1 and Fig. 2.

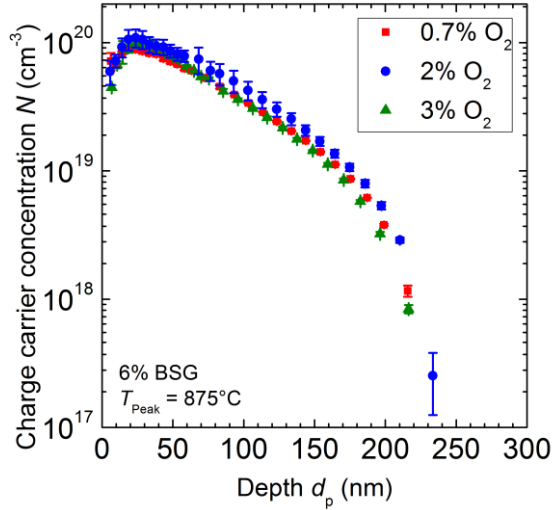


**Fig. 6:** Boron doping profiles measured by ECV (wafer center) on SDE surfaces for BSG layers with 6% concentration and diffusion processes with different peak temperatures  $T_{\text{Peak}}$ , all with an O<sub>2</sub> concentration of 0.7% in the diffusion atmosphere. The measured sheet resistances  $R_{\text{sh}}$  (center, 4pp) are given as well.

With increasing temperature, the profile depth  $d_p$  increases from  $d_p \approx 240 \text{ nm}$  at  $T_{\text{Peak}} = 875^\circ\text{C}$  to  $d_p \approx 540 \text{ nm}$  at  $T_{\text{Peak}} = 950^\circ\text{C}$ . The maximum carrier concentration  $N_{\text{max}}$  for the diffusions with  $T_{\text{Peak}} = 875^\circ\text{C}$  and  $T_{\text{Peak}} = 900^\circ\text{C}$  is  $N_{\text{max}} \approx 9 \times 10^{19} \text{ cm}^{-3}$  and increases slightly to  $N_{\text{max}} \approx 1 \times 10^{20} \text{ cm}^{-3}$  for  $T_{\text{Peak}} = 950^\circ\text{C}$ . Accordingly, the sheet resistance  $R_{\text{sh}}$  reduces from  $R_{\text{sh}} = 134 \Omega/\text{sq}$  at  $T_{\text{Peak}} = 875^\circ\text{C}$  to  $R_{\text{sh}} = 44 \Omega/\text{sq}$  at  $T_{\text{Peak}} = 950^\circ\text{C}$ . All profiles show a slightly depleted surface concentration due to segregation of boron into the oxide surface layer [10,11].

### 3.2 Influence of O<sub>2</sub> concentration on boron concentration

The impact of the O<sub>2</sub> concentration during the thermal process on boron diffusion from APCVD BSG layers is discussed for  $T_{\text{Peak}} = 875^\circ\text{C}$ . Doping profiles resulting after these diffusion processes are shown in Fig. 7, see Fig. 1 and Fig. 2.



**Fig. 7:** Boron doping profiles measured by ECV (wafer center) on SDE surfaces for BSG layers with 4.5% and 6% concentration and high-temperature processes with  $T_{\text{Peak}} = 875^\circ\text{C}$  and different O<sub>2</sub> concentrations in the process atmosphere.

All measured doping profiles show a high agreement. The boron doping is characterized by  $N_{\text{max}} \approx 9 \times 10^{19} \text{ cm}^{-3}$  and  $d_p \approx 240 \text{ nm}$ . However, the highest oxygen concentration of 3% shows the strongest surface depletion, which is reasonable, since high oxygen concentrations enhance the oxide growth and boron segregation into the oxide [11,10].

The  $R_{\text{sh}}$  measurements by 4pp (see Table I) reveal slight differences of the processes.

**Table I:** Sheet resistance measurements (4pp) of the boron-doping on 156mm n-type wafers with 400 measurement points per wafer by 4pp. The given data is organized in  $R_{\text{sh}}$  on the center of the Si wafer, average  $R_{\text{sh}}$  over the wafer surface and standard deviation.

sample	$R_{\text{sh}}$ center [ $\Omega/\text{sq}$ ]	$R_{\text{sh}}$ average [ $\Omega/\text{sq}$ ]	$R_{\text{sh}}$ std. dev. [ $\Omega/\text{sq}$ ]
4.5% BSG 0.7% O <sub>2</sub>	128	142	41
6% BSG 0.7% O <sub>2</sub>	134	131	11
6% BSG 2% O <sub>2</sub>	114	116	9
6% BSG 3% O <sub>2</sub>	135	163	71

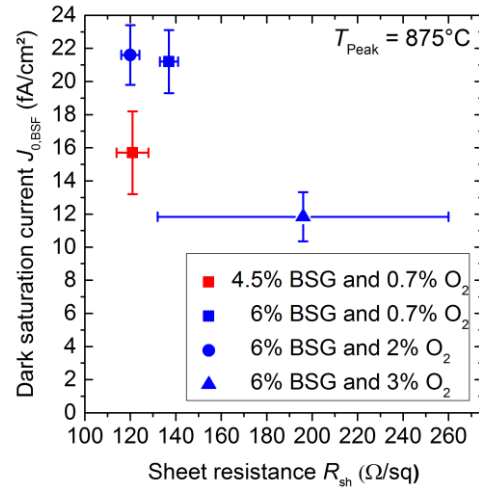
For the process with 0.7% O<sub>2</sub> content, increasing the boron concentration from 4.5% to 6% reduces the average  $R_{\text{sh}} = (131 \pm 41) \Omega/\text{sq}$  to  $R_{\text{sh}} = (131 \pm 11) \Omega/\text{sq}$  and increases the homogeneity of  $R_{\text{sh}}$ . If the O<sub>2</sub> concentration is increased to 2% and higher, no boron diffusion can be observed for a BSG layer with 4.5%. In contrast, for a BSG layer with 6% content,  $R_{\text{sh}}$  slightly reduces from

$R_{\text{sh}} = (131 \pm 11) \Omega/\text{sq}$  to  $R_{\text{sh}} = (116 \pm 9) \Omega/\text{sq}$ , whereas a further increase from 2% to 3% O<sub>2</sub> concentration again increases  $R_{\text{sh}} = (163 \pm 71) \Omega/\text{sq}$ . The inhomogeneous distribution of  $R_{\text{sh}}$  is observed on the border of the Si wafer.

In conclusion, high O<sub>2</sub> concentrations tend to increase the sheet resistance. Additionally the non-uniformity of the sheet resistance over the Si-wafer is increased if the O<sub>2</sub> concentration is increased. We attribute these effects to a thermally grown SiO<sub>2</sub> layer at the interface Si-wafer to BSG layer. This SiO<sub>2</sub> layer acts as diffusion barrier against boron from BSG layer and even leads to complete decoupling of the BSG layer for higher oxygen concentrations.

### 3.3 Dark saturation current densities for diffusion processes with peak temperature of 875°C.

Dark saturation current densities  $J_{0,\text{BSF}}$  for boron BSF diffusion processes with  $T_{\text{Peak}} = 875^\circ\text{C}$  (section 2.1 Fig. 2 and Fig. 3) are shown in Fig. 8.



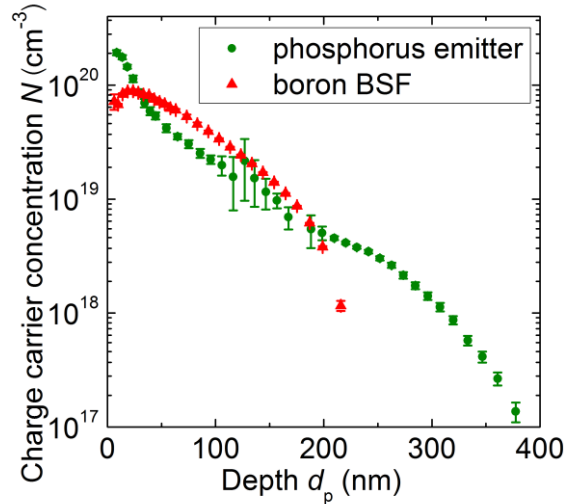
**Fig. 8:** Dark saturation current density  $J_{0,\text{BSF}}$  (planar surface, AlO<sub>x</sub>/SiN<sub>x</sub>-passivation, average and standard deviation of five measurement points per wafer) over average value of sheet resistance  $R_{\text{sh}}$  (average  $R_{\text{sh}}$  measured by means of inductive coupling using an inline tool [12]) for diffusion processes at  $T_{\text{Peak}} = 875^\circ\text{C}$ .

The observed recombination currents are very low and range from  $J_{0,\text{BSF}} = (22 \pm 2) \text{ fA}/\text{cm}^2$  at  $R_{\text{sh}} = (121 \pm 7) \Omega/\text{sq}$  to  $J_{0,\text{BSF}} = (12 \pm 1) \text{ fA}/\text{cm}^2$  for  $R_{\text{sh}} = (196 \pm 64) \Omega/\text{sq}$ . The graph shows average  $R_{\text{sh}}$  measured by means of inductive coupling using an inline tool [12].

With respect to a homogeneous distribution of the sheet resistance 4.5% boron concentration and 0.7% O<sub>2</sub> concentration as well as 6% boron concentration and 3% O<sub>2</sub> concentration are not well suited for the fabrication of PERT cells. Thus, for the fabrication of co-diffused PERT cells 6% boron content and a diffusion process with an O<sub>2</sub> concentration of 0.7% are selected.

### 3.3 Characterization of full co-diffusion process

Based on 6% boron concentration in the BSG layer and 0.7% O<sub>2</sub> content in the diffusion atmosphere the final co-diffusion process shown in Fig. 4 is developed. The resulting doping profiles measured by ECV are shown in Fig. 9.

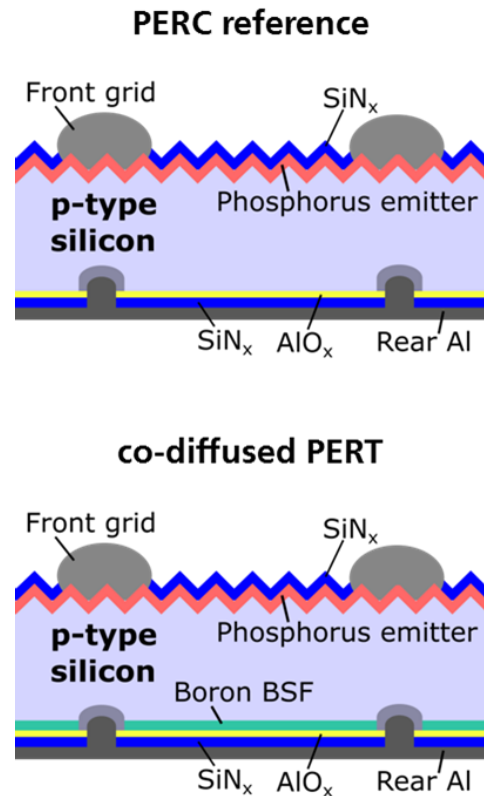


**Fig. 9:** ECV measurement of the co-diffusion process for simultaneous boron diffusion (red symbols) from an APCVD BSG/SiO<sub>x</sub>-layer stack and phosphorus diffusion (green symbols) from a POCl<sub>3</sub> ambient.

The samples are processed as described in section 2.1 Fig. 3. The Phosphorus doped emitter is characterized by  $N_{\max} \approx 2 \times 10^{20} \text{ cm}^{-3}$  and  $d_p \approx 380 \text{ nm}$ . This results in  $R_{\text{sh}} = (90 \pm 2) \Omega/\text{sq.}$  measured by means of inductive coupling using an inline tool [12] and  $J_{0e} = (79 \pm 15) \text{ fA/cm}^2$  for an alkaline textured and passivated (SiN<sub>x</sub>) surface.

### 3.3 Comparison PERC and co-diffused PERT solar cells

Based on the developed co-diffusion process (Fig. 4) monofacial PERT cells are fabricated and compared to monofacial PERC cells based on standard POCl<sub>3</sub> diffusion process developed at Fraunhofer ISE [9]. Fig. 10 illustrates the different cell structures which are fabricated according to the process plan in Fig. 5.



**Fig. 10:** Investigated PERC and PERT cell structures fabricated according to the process plan in Fig. 5. PERT cells are fabricated with a POCl<sub>3</sub>-based co-diffusion process (see Fig. 4). For the PERC cells a standard POCl<sub>3</sub> based diffusion process is used [9].

The results of IV measurements using an industrial cell tester for the different cell types are presented in Table II.

**Table II:** IV data (as processed) for PERC and PERT solar cells with an edge length of 156 mm and  $\rho_B = 2.9 \Omega\text{cm}$  using an industrial cell tester. Shown are the median values of best peak firing temperature groups.

Cell type	$V_{oc}$ [mV]	$J_{sc}$ [mA/cm <sup>2</sup> ]	$FF$ [%]	$\eta$ [%]	$R_p$ [k $\Omega\text{cm}^2$ ]	$R_s$ [ $\Omega\text{cm}^2$ ]
PERC reference	653	39.6	79.3	20.5	109	0.5
PERT co-diff.	649	39.4	80.3	20.5	52	0.4

Median values of best groups of PERC and PERT cells are shown. The PERC reference cells show 4 mV higher  $V_{oc}$  and 0.2 mA/cm<sup>2</sup> higher  $J_{sc}$ . This is attributed to an increased rear surface recombination of the PERT cells. Control samples of this batch showed an increased  $J_{0,BSF} = (152 \pm 35) \text{ fA/cm}^2$ , much higher than observed in previous runs (see Fig. 8). The lateral conductance of the BSF increases the  $FF$  of the PERT cells by 1%<sub>abs</sub> to  $FF = 80.3\%$ . Thus, both cell types show the same efficiency level of  $\eta = 20.5\%$ . Peak efficiencies are 20.7% for PERC and 20.6% for PERT.

#### 4 SUMMARY AND CONCLUSION

We investigate boron doping from APCVD BSG/SiO<sub>x</sub> layer stacks. At moderate diffusion conditions of 875°C for 30 min, average sheet resistances of  $R_{sh} = 116$  to  $163 \Omega/\text{sq}$  are observed with low recombination parameters of  $J_{0,\text{BSF}} = 22$  to  $12 \text{ fA}/\text{cm}^2$ , respectively (planar surface Al<sub>2</sub>O<sub>3</sub>/SiN<sub>x</sub> passivation). With these conditions, we develop a POCl<sub>3</sub>-based co-diffusion process leading to a simultaneous phosphorus-diffusion of  $R_{sh} = (90 \pm 2) \Omega/\text{sq}$ , measured by inline- $R_{sh}$  measurement and  $J_{0e} = (79 \pm 15) \text{ fA}/\text{cm}^2$ . Finally, we prove the co-diffusion concept by fabricating monofacial PERT solar cells with peak efficiencies of 20.6% and 20.5% (median value) on 156mm 2.9  $\Omega\text{cm}$  p-type Cz-substrates.

In conclusion, co-diffusion using APCVD BSG layers and POCl<sub>3</sub>-diffusion is a promising approach for PERT cell fabrication, enabling high quality boron BSF formation with excellent recombination properties. Relevant applications are bifacial PERT cells with increased rear efficiency due to reduced shading as well as minimization of LID due to high tolerance of PERT cells to high resistivity wafers.

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